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WEAR PARTICLE ANALYSIS OF GREASE SAMPLES. (U)
APR 79 E R BOWEN, J P BOWEN

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NAVAL AIR ENGINEERING CENTER

REPORT NAEC-92-129

WEAR PARTICLE ANALYSIS OF GREASE SAMPLES

Handling and Servicing/Armament Division
Ground Support Equipment Department
Naval Air Engineering Center
Lakehurst, New Jersey 08733

18 APRIL 1979

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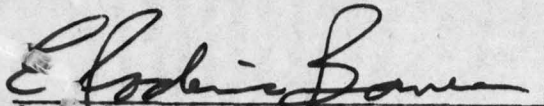
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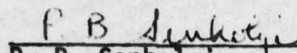
WEAR PARTICLE ANALYSIS OF GREASE SAMPLES

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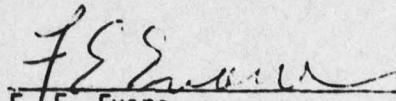
J. M. Bowen/E. Roderic Bowen
Foxboro Analytical Division
The Foxboro Company

Reviewed by:



P. B. Senholzi
Handling and Servicing/Armament
Division (927)

Approved by:



F. E. Evans
Ground Support Equipment Superintendent

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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) An investigation was conducted to analyze a number of widely used types of grease samples by Ferrography. Solvent systems were successfully formulated to dissolve these greases for analytical purposes. A number of grease samples from aircraft components were subjected to Ferrographic analysis and results reported. | | |

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SUMMARY

The use of wear particle analysis for monitoring or diagnosing the condition of oil-lubricated bearings is now well established, and because many critical bearings are lubricated with grease, an investigation was authorized to assess the extent to which the use of this technology could be widened to cover grease-lubricated bearings.

During normal operation, only a small proportion of the grease within a bearing plays a significant part in its lubrication. Particles arising from wear are, therefore, very unevenly distributed. Accordingly, it was decided that the sample should be taken from the actual component wear track. This would be dissolved in a suitable fluid from which samples might be selected for use in the same way as with oil-lubricated systems.

A number of solvents were investigated both singly and in combination and a blend consisting of 30% toluol and 70% hexane was shown to be suitable, particularly when mixed with its own volume of diester based lubricant (to MIL-L-23699 specifications).

Ferrography was utilized as the prime wear particle analysis technique. Heating the Ferrogram to 625°F (330°C) for 90 seconds was shown to permit more satisfactory examination and analysis of metallic wear particles because it eliminated an organic residue which was sometimes present.

The use of the aforementioned solution is recommended, but care in handling the solvent is necessary because of the low flash point of hexane.

A number of Ferrograms relating to bearings used in helicopters were obtained with complete success.

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I. INTRODUCTION

A. WEAR PARTICLE ANALYSIS TECHNOLOGY ADAPTATION TO GREASE-LUBRICATED

COMPONENTS. Wear particle analysis is now a well developed technology for the study of oil-lubricated systems. Critical wear particle parameters defined under this technology are concentration, size distribution, composition and morphology. The monitoring of these parameters in oil-lubricated systems is for the most part straightforward. Many wear components, however, are lubricated with grease and at the present time there exists no acceptable procedures for monitoring the wear condition of such components.

The nature of the grease lubricant creates several problems with respect to the monitoring of the above mentioned four critical wear particle parameters. The main difficulty is that a simple measurement of the wear metal concentration in a grease sample does not necessarily reflect the wear condition of the lubricated component. There are at least two reasons for this situation. First, the products of wear are not distributed uniformly in the grease. Hence, a grease sample will not necessarily reflect the total wear product concentration. Second, the products of wear do not leave the component and consequently the wear particle concentration will increase with time. Thus the equilibrium concentration, characteristic of oil-lubricated systems, does not exist in grease-lubricated systems.

As a result of the concentration measurement difficulties, grease wear particle analysis will be forced to rely heavily on the remaining three critical parameters of size distribution, composition and morphology.

The objective of this research effort is to develop techniques for the study of wear particles/wear particle parameters in grease-lubricated systems as well as trends with respect to analysis criteria.

Wear particle critical parameters are monitored under this effort by use of the well documented technique of Ferrography. Ferrography will thus receive major emphasis in the following summary report.

B. USE OF GREASES IN AIRCRAFT EQUIPMENT. The decision of the designer as to whether to use oil or grease as a lubricant depends on the operating conditions of the system to be lubricated, particularly the mechanical and thermal aspects. Greased bearings have come into very wide use for mechanisms which are widely separated physically, such as the wheel bearings on automobiles or control surface bearings in aircraft. Modern sealed greased bearings exhibit long life, and in many applications, are economically attractive with respect to both initial and maintenance costs. Many other mechanisms such as splines and hinges are commonly grease-lubricated. Recently, high-powered helicopter gear trains have been successfully lubricated with grease.

C. CHARACTERISTICS OF GREASE FORMULATIONS. Greases are two-phase systems incorporating a liquid and a solid phase. They possess a gel structure with characteristic rheological properties which are determined by the type and concentration of the thickener, the type of lubricating oil, and the amount and properties of materials added to the grease to achieve specific

characteristics. The thickener may be a soap, an organic compound, a complex material made up of organic and inorganic compounds, or a combination of these. Greases are thus very complex and numerous variables affect their physical and chemical characteristics, and in turn their performance in service.

D. CHARACTERISTICS OF GREASE PERFORMANCE. The factors affecting the grease performance in service are many and include temperature, contact with metals, contamination by dirt or moisture, and bearing stresses. These factors can affect either one or more components (oil, thickeners, or additives) of the greases.

Observations on the movement and structure of grease in roller bearings¹ have shown that in a grease-lubricated roller bearing, only the small amount of grease between the rollers and races provide the lubrication. The pockets of grease held by the retainer are relatively inactive. The principal role of the grease in the pockets appeared to be to keep in position the small amount of material responsible for lubrication and to replenish the oil as it is lost by evaporation or degradation. Thus, in a correctly operating grease-lubricated bearing, a small amount of grease becomes severely worked and degraded, whereas the bulk of the grease remains in an almost virgin state.

The movement of wear particles in a grease-lubricated part is restricted to the region where the active grease is located. Therefore, a basic problem in monitoring grease-lubricated parts is that the simple measurement of the concentration of an element in the bulk grease provides no information regarding the wear rate. This occurs because the concentration of wear particles is not uniform throughout the grease and varies with the place from which the grease was sampled.

E. SELECTION OF GREASE SOLVENT SYSTEMS. In order to apply the techniques of Ferrography to grease-lubricated bearings, two aspects have to be considered. First it is necessary to discover a solvent which will dissolve the grease sample so as to produce a fluid of suitable viscosity for Ferrographic examination. Second, it must be demonstrated that the particles found in the grease are accurately represented in the fluid sample.

Because the ingredients used in grease formulations are diverse, the selection of a single solvent for all greases appears to be a difficult task. Solid additives incorporated in greases are insoluble. A wide variety of soaps or thickeners may be used by different manufacturers with the same liquid lubricant to comply with specific grease requirements and the same specifications. Further differences in greases from manufacturer to manufacturer may result from differences in manufacturing procedures. For example, one manufacturer may use a soap base to thicken a specific lubricating fluid, while another may incorporate the soap-making procedure in the grease manufacturing process.

¹ A. A. Milne, D. Scott, and H. M. Scott "Observations on the Movement and Structure of Grease in Roller Bearings", Proc. Conf. on Lubrication and Wear, 1957. 450-453 and 893. Inst. Mech. Engrs., London, 1958.

The concentration, distribution and size of the solid phases may also vary in unused greases.

F. DEVELOPMENT OF RELIABLE GREASE SAMPLING/ANALYSIS TECHNIQUES. It was therefore necessary to establish a reliable technique for sampling grease and to select solvents which could be used to dissolve greases of all types. It was also necessary to demonstrate that once a sample of grease had been treated with a suitable solvent, that the same wear particle monitoring trends could be used as have been successfully applied to the analysis of oil samples.

II. SELECTION OF SOLVENTS BASED ON UNUSED GREASES

A. GREASE FORMULATIONS SELECTED FOR STUDY. In order to conduct solvating studies covering a range of combinations of ingredients in the more commonly employed greases, samples were obtained of the nine greases listed in Table 1. Their basic ingredients and specific uses are given. The nine greases cover a range of fluid lubricants, soap phases, and solid additives.

B. GREASE SOLVENT SYSTEMS SELECTED FOR STUDY. Three solvent systems were initially chosen for solvation studies on the nine unused greases. As the solvency power of a solvent system on different materials cannot be accurately predicted, the three solvent systems chosen had varying balances of polar, nonpolar, and aromatic or aliphatic constituents. The solvents are listed in Table 2.

The initial solvation studies were conducted with the first four greases listed in Table 1. These were reported to be the greases most used in service.

C. SOLVATING TEST METHODS. The solvating test method chosen was to introduce ten 3-mm-diameter glass beads into a standard Ferrographic sample bottle, the capacity of which is 1/2 U.S. fluid ounce (15 ml). A small amount, approximately .1 cc, of grease and 10 ml of the solvent to be tested were added. The bottle was then sealed and well shaken by hand. Previous experience had indicated that the use of glass beads considerably shortened the time of agitation required for grease solution and exhibits no negative effects on particle analysis.

A Ferrograph was prepared from 2 ml of the contents of the bottle immediately after shaking. Following the pumping of the grease solvent mixture, the Ferrogram was washed by pumping the pure solvent over the Ferrogram. The Ferrogram was washed by passing the test solvent over it for 10 minutes.

Summarized test results on the unused greases and different solvent systems are given in Table 3.

D. INITIAL RESULTS OF SOLVATING TESTS WITH DIFFERENT UNUSED GREASE

FORMULATIONS. Solvent #1 was found to be ineffective in lithium soap greases. For record purposes, photomicrographs of undissolved grease deposits on Ferrograms of lithium soap greases are shown in Photos Nos. F1428-1 to -6 (appendix B, pages 29(B-1) to 31(B-3)). Heating of the Ferrogram to 625°F was ineffective in removing the undissolved lithium soap, Photo No. F1423-32 (appendix B, page 45(B-17)).

Solvent #2, incorporating three liquids (toluol/MEK/isopropanol) was considered to be a potentially more powerful solvating medium than Solvent #1, as mixtures of solvents generally produce synergistic effects. It is often found that a material insoluble in either of two solvents is soluble in a mixture of the solvents. However, Solvent #2 was found to be a less effective solvent for lithium soap greases than Solvent #1. It is evident that lithium soap greases resist solvation in highly polar/aromatic solvent systems.

Solvent #3, containing less aromatic solvent (30% toluol) and more non-polar aliphatic solvent (70% hexane), proved to be effective for the solution of lithium soap/petroleum oil type grease as shown in Photos Nos. F1437-7 and -8 (appendix B, page 32(B-4)). This solvent was therefore used to treat the remaining grease samples.

E. FERROGRAPHIC ANALYSIS OF DIFFERENT TYPES OF GREASE SAMPLES. Ferrograms of certain grease samples, but especially those from Sample #4, a lithium soap silicone grease, contained particulate matter as shown in Photos Nos. F1442-13 to -18 (appendix B, pages 35(B-7) to 37(B-9)). Consultation with the grease manufacturer revealed that the lithium soap silicone grease contained approximately three times the amount of lithium soap (up to 35%) than that contained by a petroleum oil lithium soap grease. It was also suggested that the white lumps seen on the Ferrograms, Photos Nos. F1442-15 and -16 (appendix B, page 36(B-8)), were particles of the original soap rather than additive material. It was postulated that service use of this grease caused the soap particles to flatten out. Such modified particles were observed on Ferrograms prepared from worked grease as shown in Photos Nos. F1491-36 to -39 (appendix B, pages 47(B-19) and 48(B-20)).

Particulate matter was also found on Ferrograms prepared for grease Samples #6 and #7 containing molybdenum disulphide and for grease Sample #8, a barium soap grease. The Ferrogram prepared from the latter type of grease contained an organic-type network which was eliminated by heating the Ferrogram to 625°F for 90 seconds as shown in Photos Nos. F1443-26 to -31 (appendix B, pages 42(B-14) to 44(B-16)). Diluting the grease volumetrically 10:1 with Solvent #3 dispersed the weblike organic material as shown in Photos Nos. F1479-33 and -34 (appendix B, pages 45(B-17) and 46(B-18)). A volumetric dilution is preferable since an increased error due to particulate density effects in heavily contaminated samples is minimized.

The presence of molybdenum disulphide in the grease (Samples #6 and #7) caused problems. The large particles of molybdenum disulphide settled on the bottom of the sample bottle and did not transfer to the Ferrogram. This problem was overcome by mixing the solvent-treated sample with equal parts of a diester fluid (MIL-L-26399) as can be seen from Photos Nos. F1440-21, -22 and -23 (appendix B, pages 39(B-11) and 40(B-12)).

A second problem was that the large particles of molybdenum disulphide could obscure wear particles precipitated from the grease onto the Ferrogram. The morphology of the molybdenum disulphide particles was significantly changed by test working of the grease. The change of morphology is discussed under solvation studies of used greases.

Grease #7, with a lower concentration of molybdenum disulphide, caused no problem. Photos Nos. F1478-9 and -10 (appendix B, page 33(B-5)) show typical Ferrograms prepared from this grease.

Greases #3, #5, #7 and #9 were effectively dissolved by Solvent #3. Photos Nos. F1439-11 and -12 (appendix B, page 34(B-6)) show typical Ferrograms prepared from grease #3 which contained a diester fluid with a silicone

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thickener. Photos Nos. F1434-19 and F1438-20 (appendix B, page 38(B-10)) show comparative Ferrograms prepared from grease #5 containing petroleum oil with an aluminum complex soap with Solvent #2 and #3 respectively. Photos Nos. F1441-24 and -25 (appendix B, page 41(B-13)) show typical Ferrograms prepared from grease #7 containing petroleum oil thickened with a Bentone clay and molybdenum disulphide. Photo No. F1474-35 (appendix B, page 46(B-18)) shows a typical Ferrogram prepared from grease #9 which contained petroleum oil and a calcium soap and which is completely clear except for "dirt" particles.

III. WORKED GREASES

A. TEST MACHINE CONDITIONS. The three unused greases found most difficult to dissolve for Ferrographic analysis procedures #4, #6 and #8 were subjected to working in a test machine before being used for further solvation studies. The grease working test consisted of rubbing an AISI 52100 steel race against a fixed steel bearing ball under a load of 80 lb/in.² for 2 minutes. A small quantity of unused grease was used for each test. Small samples of each worked grease were treated with Solvent #3 according to the procedure described for the unused grease samples (paragraph II.C). Ferrograms were prepared from each sample. Table #4 summarizes the data produced in these tests.

B. FERROGRAPHIC ANALYSIS OF CERTAIN TYPES OF WORKED GREASES. As already shown in Photos Nos. F1491-36 to -39 (appendix B, pages 47(B-19) and 48(B-20)), working of the lithium soap silicone grease #4 reduced the size of the undissolved particulate matter deposited on the Ferrogram, and also eliminated its interference with the interpretation of the Ferrogram. Even in the presence of a background of undissolved grease, wear particles precipitated from the grease can be satisfactorily analyzed by bichromatic microscopy.

For satisfactory Ferrogram preparations from grease sample #6, containing a large particle size molybdenum disulphide additive, it was necessary to dilute the sample by the addition of a diester fluid, MIL-L-23699. Photos Nos. F1493-40 and -41 (appendix B, page 49(B-21)) show the few particles on Ferrograms prepared from the unworked grease without dilution with the diester fluid. Photos Nos. F1494-42 and -43 (appendix B, page 50(B-22)) show metallic wear particles precipitated on the Ferrogram prepared from the worked grease sample diluted with diester fluid.

C. SPECIAL TECHNIQUES IN ELIMINATING ORGANIC BACKGROUND MATERIAL ON

FERROGRAMS. The background network of organic material found on Ferrograms prepared from unused barium soap base petroleum oil grease #8 was also found on Ferrograms prepared from worked samples of the same grease, but to a lesser extent. Particles forming the network were also reduced in size, see Photos Nos. F1492-44 and -45 (appendix B, page 51(B-23)). Heating of the Ferrogram to 625°F (330°C) for 90 seconds eliminated the organic material to allow more satisfactory examination and analysis of the metallic wear particles (see Photo No. F1492-46, appendix B, page 52(B-24)).

IV. EXAMINATION OF SAMPLES TAKEN FROM GREASE LUBRICATED SYSTEMS OF AIRCRAFT, NAVAL AIR REWORK FACILITY (NARF), SAN DIEGO, CALIFORNIA

A. TYPES OF AIRCRAFT AND SAMPLES. A number of samples were taken from critical areas of fixed-wing aircraft and helicopters at the Naval Aircraft Rework Facility (NARF), San Diego, California, and subjected to Ferrographic analysis at Foxboro Analytical. Particulars of these samples are summarized in Table 5 and photographs of the Ferrograms are also reproduced.

This report does not purport to include a definitive account of the conclusions to be drawn from the examination of the respective aircraft components, but the observations are reported as evidence of the potentiality of grease wear particle analysis techniques.

B. FERROGRAPHIC ANALYSIS OF AIRCRAFT GREASE SAMPLES (TABLE 5). The field sample Ferrogram photograph, No. F1940-1 (appendix B, page 53(B-25)), (E2 landing gear nosewheel sample) reveals translucent material which is accounted for by soap remaining from degradation of the grease, but appears to be exceptional insofar as the majority of the Ferrograms do not exhibit this feature. Where it does occur, it is readily identifiable and is easily distinguished from wear particles. This example also emphasizes the care necessary in sampling because of the risk of contamination of the grease from external sources. The metallic particles in Photo No. F1940-1 probably originate in this manner. On the other hand, those in Photo No. F1943-1 (appendix B, page 53(B-25)) are probably wear particles because they occur in grease removed directly from the race.

A similar sample from the race of a tapered roller bearing, of a landing gear nosewheel, showed free metal particles and was free of residual grease (see Photo F1964-1, appendix B, page 54(B-26)).

A number of samples which were taken from the swash plate assembly of an H53 helicopter again serves to emphasize the critical nature of the sampling process. A sample taken from behind the spaces between the two rolling bearings, revealed a surprising number of severe wear particles (see Photo No. F1946-1, appendix B, page 55(B-27)) whereas a sample taken from around the ball of the upper bearing showed heavy deposits of friction polymer (see Photo No. F1966-1, appendix B, page 55(B-27)). However, a sample taken from the grease exuded from under the assembly seals (Photo No. F1965-1, appendix B, page 54(B-26)), contained mostly contaminants and non-wear related debris.

Samples from a helicopter reduction gear showed a certain amount of cutting wear in a sample taken from the planetary gear teeth (Photo No. F1987-1, appendix B, page 62(B-34)).

The stationary splines at the rotor head of the H46 helicopter were investigated (Photos Nos. F1960-1, F1961-1 and F1962-1, appendix B, pages 63(B-35) and 64(B-36)). Grease taken from the spline showed severe wear particles. The similarity of Ferrograms (Photos Nos. F1961-1 and F1962-1) suggest that the particle distribution does not vary alarmingly along the wear track of an individual component.

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Samples from the tail rotor drive spline of the CH 53A aircraft (Photos Nos. F1990-1 and F1991-1, appendix B, page 65(B-37)) revealed no evidence of serious wear, but the sample was very dirty, presumably due to the fact that the components are open to environment when the craft is in the parked position. (When running, the components are protected by O-ring seals.)

V. DISCUSSION

A. FEASIBILITY OF FERROGRAPHIC ANALYSIS OF GREASE SAMPLES. The results reported in Section III demonstrate the feasibility of obtaining satisfactory Ferrograms from grease-lubricated components. The examination of such components (primarily bearings) is not, however, as straightforward as when oil is used as a lubricant for two reasons. First, the distribution of wear particles within the grease is very uneven; and second, because the physical configuration of most components precludes the extraction of grease without actual dismantling.

B. SELECTION OF GREASE SAMPLES. There will be many situations where "condition monitoring" using Ferrography will be precluded by sampling difficulties. However, in systems where sampling can be carried out readily, similar techniques to those perfected for oil-lubricated systems can be applied. In many cases, however, it will not be feasible to dismantle components for sampling, and the role of Ferrography will be restricted to failure analysis of those components which have been dismantled for one reason or another.

VI. CONCLUSIONS

- A. Grease Solvent #3 (toluol/hexane) was the most effective for use with the wide range of grease samples investigated. It appears to be potentially suitable as a general solvent for all greases. It should contain up to 50% of diester (MIL-L-23699) to suspend high-density large particle material and to prevent co-settling of wear particles (Paragraph IID).
- B. Commonly used solid additive materials such as molybdenum disulphide and carbon black (graphite) present no difficulty to Ferrographic analysis if the dissolved sample diluting procedure developed is used (Paragraph IIF).
- C. Many insoluble organic materials present in greases, if deposited on Ferrograms, may be eliminated by heating the Ferrogram after initial analysis (Paragraph IIIC).
- D. The use of glass beads to speed up the grease solvating process should be incorporated in any standard grease Ferrogram preparation procedure (Par. IIC).
- E. The use of hexane, which has a low flash point, may not be desirable. Further work on solvents could be directed towards replacing hexane with a higher flash point aliphatic material of comparable solvency power (Paragraph IID).
- F. The wash for the Ferrograms may be similar to the grease solvent. Incorporation of a material to effect quick drying may be required if a solvent of higher flash point than hexane is utilized (Paragraph IIC).
- G. Ferrograms can be made from grease-lubricated bearings of a quality which is comparable with that achievable with oil-based samples (Paragraph VA).
- H. Sampling of grease from bearings may be difficult due to lack of access. It is also important to take into account the uneven dispersion of wear particles within the bearing system. This limits quantitative analysis techniques (Paragraph VA).
- I. Samples should be taken directly from the wear track or wear surface (or as close as possible), (Paragraph IVB).
- J. The analysis should be primarily qualitative. Quantitative analysis should be performed only on a comparative basis. That is, a comparison of abnormal particles to normal particles within an individual sample. Morphology of the abnormal particles plays a primary role in all grease sample analyses (Par. IVB).
- K. Due to the high level of contaminants in fresh grease, it is essential that a Ferrogram of the fresh grease be used as a reference (Paragraph IIE).
- L. In the light of the aforementioned difficulties, Ferrography is more likely to be applicable to diagnosis of failure and as a design tool than to condition monitoring. Applications exist, however, where access to the operative regions of a bearing is readily available and where monitoring programs are both feasible and desirable.
- M. The types of wear particles present in grease samples are consistent with those found in oil-lubricated systems (Paragraph IVB).

VII. RECOMMENDATIONS

- A. It is recommended that the preceding procedures be used as a basis for standardizing the use of Ferrography for the examination of grease-lubricated components.
- B. Grease, when extracted from a bearing, should be dissolved in a solvent mixture consisting of 15% toluol, 35% hexane, and 50% diester-based lubricant.
- C. Ferrograms may be heated to 330°C (625°F) for 90 seconds to eliminate organic residue from the grease after initial analysis.
- D. Care should be taken when storing and handling the recommended solvent because of the low flash point of hexane.
- E. Further work should be pursued in the areas of sampling technique, sampling location, and wear particle analysis criteria.

TABLE 1. GREASE TYPES

| SAMPLE NO. | BASE OIL | THICKENER (SOAP) | SOLIDS (ADDITIVES) | USES/COMMENTS |
|------------|-------------------|-----------------------|----------------------|--|
| 1 | Petroleum | Lithium Soap | ----- | Reported to have the widest general purpose uses. Operating range -10 to 250°F for plain and anti-friction bearings. Molybdenum Disulfide is to improve anti-wear properties and load-bearing characteristics. |
| 2 | Petroleum | Lithium Soap | Molybdenum Disulfide | |
| 3 | Synthetic Diester | Silica | Silica | Bearings - both low and high temperature use - temperature range -40°F to 500°F. |
| 4 | Silicone | Lithium Soap | ----- | High temperature bearings, bearings in hot areas - temperature range -40°F to +450°F. Meets MIL Specification MIL-L-15719A, Amendment 3. |
| 5 | Petroleum | Aluminum Complex Soap | ----- | Extreme pressure bearings and gear-type couplings, also multipurpose. Good water and oxidation resistance. Operating range 0°F to 400°F, intermittent up to 450°F. |
| 6 | Petroleum | Mixed (Proprietary) | Molybdenum Disulfide | Heavy duty use, Molybdenum Disulfide to improve load-bearing characteristics. Primary uses (#6) open gears, (#7) couplings. Has "no-drip" characteristics, range 25°F to 400°F. |
| 7 | Petroleum | Clay (Bentone) | Molybdenum Disulfide | |

(continued ...)

Table 1 (continued)

| SAMPLE NO. | BASE OIL | THICKENER (SOAP) | SOLIDS (ADDITIVES) | USES/COMMENTS |
|------------|-----------|---------------------|--------------------|---|
| 8 | Petroleum | Barium Complex Soap | ----- | Multipurpose lubricant, high water resistance. Used for marine, construction, mining. Temperature range 0°F to 250°F. |
| 9 | Petroleum | Calcium Soap | ----- | Extreme pressure lubricant for gears in bath, semi-fluid type. Temperature range 0°F to 150°F. |

TABLE 2. GREASE SOLVENT SYSTEMS SELECTED FOR STUDY

1. GREASE SOLVENT #1
toluol (50%), isopropanol (50%)
an aromatic/polar blend
2. GREASE SOLVENT #2
toluol (33%), methyl ethyl ketone (MEK) (33%), isopropanol (34%)
an aromatic higher polar blend
3. GREASE SOLVENT #3
toluol (30%), hexane (70%)
an aromatic, aliphatic, essentially nonpolar blend

TABLE 3. SUMMARY - SOLVATION STUDIES - VARIOUS GREASE TYPES (FRESH)

| SAMPLE NO. | SOLVENT/WASH | FERROGRAM NUMBER | PHOTO NUMBER | RESULTS | COMMENTS/SIGNIFICANCE |
|--|--------------|---------------------|---------------------------|---|--|
| No. 1 Lithium Soap | Solvent #1 | Fl428 | Fl428 -1 to -6 | Solvent #1 (Toluol/ Isopropanol). Not effective with Lithium soap greases. | Highly polar, aromatic solvent systems are inad- equate. (Also, see Photo Fl423-32). |
| No. 1 Lithium Soap | Solvent #3 | Fl437 | Fl437 -7 & -8 | Solvent #3 (Toluol/ Hexane). Appears to be effective in dissolving grease and Lithium Soap. Only insoluble particu- late matter visible. | A solvent system with a high aliphatic content is required for complete removal of greases and soap on substrates. |
| No. 2 Lithium Soap plus Moderate MoS2 Content | Solvent #3 | Fl478 | Fl478 -9 & -10 | Grease and soap dissolv- ed. MoS2 particles were precipitated. Some non- metallic transparent spheres were observed on the Ferrogram. | The low level of the MoS2 content on the Ferrogram would not obscure metallic particles in used grease. Heavy duty greases with high MoS2 content may present a problem. |
| No. 3 Diester Base Oil with Silica | Solvent #3 | Fl439 | Fl439 -11 & -12 | Substrates show no grease or oils, minor amounts of Silica. | This diester base oil sample solvates very well in Sol- vent #3. No special prob- lems observed. |
| No. 4 Silicone Base Oil with Lithium Soap | Solvent #3 | Fl422 | Fl442 -13 to -18 | Large amount of insolu- ble grease, soap, and particulate matter. Some particles up to 200 μ m. | High soap content (up to 35%) plus particulate matter may make Ferrographic analysis difficult. Refer to used Silicone grease tests. |

(continued ...)

Table 3 (continued)

| SAMPLE NO. | SOLVENT/WASH | FERROGRAM NUMBER | PHOTO NUMBER | RESULTS | COMMENTS/SIGNIFICANCE |
|---|---------------------------------------|---------------------|---------------------------|--|--|
| No. 5 Aluminum Complex Soap | Solvent #2 | Fl434 | Fl434 -19 | Some grease or soap residue evident at entry. | This Solvent, #2, not efficient in solvating action. Compare to Fl438 below with Solvent #3 system. |
| No. 5 Aluminum Complex Soap | Solvent #3 | Fl438 | Fl438 -20 | Substrate free of grease or soap. Only minor particulate matter evident. | Grease Solvent #3 effective with this type of grease. |
| No. 6 MoS ₂ Solids | Solvent #3 | Fl440 | Fl440 -21 | Very little MoS ₂ deposi- ted on substrate having settled in dissolved sample and turret tube. | Fresh greases with large particles (50 μ m range) will not necessarily show the particles on substrate. Compare to Fl444 below. |
| No. 6 MoS ₂ Solids | Solvent #3/ MIL-L-23699 (50-50) | Fl444 | Fl444 -22 & -23 | Large (50 μ m) particle size MoS ₂ suspended by oil/solvent mixture. | The amount and size of MoS ₂ particles will interfere with Ferrogram analysis. A solvent mixture required suspended MoS ₂ particles. |
| No. 7 MoS ₂ Solids plus Clay | Solvent #3 | Fl441 | Fl441 -24 & -25 | The medium size (5-20 μ m) MoS ₂ particles deposit in large quantities on substrate. Clay (Ben- tone) also deposited. | MoS ₂ particles obscure entry deposit area. |
| No. 8 Barium Complex Soaps | Solvent #3 | Fl443 | Fl443 -26 to -31 | Large network of non- metallic material very heavy at entry and dis- tributed throughout substrate. | Organic material will ob- scure metallic deposits. Heat to 625°F (Fl443-29, -31) clarifies or evapor- ates the material. |

(continued ...)

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Table 3 (continued)

| SAMPLE NO. | SOLVENT/WASH | FERROGRAM NUMBER | PHOTO NUMBER | RESULTS | COMMENTS/SIGNIFICANCE |
|------------------------------------|--------------|---------------------|-----------------------|---|---|
| No. 1 Lithium Soap | Solvent #1 | Fl423 | Fl423 -32 | Heating Ferrogram to 625°F for 90 seconds does not remove undis- solved grease. | Refer to Photos Fl428-1 thru -6. |
| No. 8 Barium Complex Soap | Solvent #3 | Fl479 | Fl479 -33 & -34 | Dilution (10:1 ratio) reduces agglomerated non-metallic mass to isolated strings, but has tendency to catch on metallic particles (Photo Fl479-34). | Dilution appears to free substrate from this organic matter, but effect on used greases would have to be checked. |
| No. 9 Calcium Soap | Solvent #3 | Fl474 | Fl474 -35 | Substrate free of soap or grease. | Solvent #3 appears satis- factory for this type of grease. |

TABLE 4. SUMMARY - SOLVATION STUDIES - VARIOUS GREASE TYPES (WORKED)

| SAMPLE NO. | SOLVENT | FERROGRAM NUMBER | PHOTO NUMBER | RESULTS | COMMENTS/SIGNIFICANCE |
|------------------------------------|---|---------------------|---------------------------|--|--|
| No. 4 Silicone Grease | Solvent #3 | Fl491 | Fl491 -36 to -39 | Photos Fl491-36 to -39 show deposits in fresh grease are minimized. Bichromatic illumination may be employed to identify metallic wear particles | Use of Bichromatic light or microscope analysis of Ferrograms of used Silicone grease samples should be confirmed as standard technique. |
| No. 6 Molybdenum Disulfide | Solvent #3 | Fl493 | Fl493 -40 & -41 | Photos Fl493-40 and -41 have no metallic wear particles, few MoS ₂ particles. | 50 μ m or larger MoS ₂ particles settled too fast for Ferrograph pumping. |
| No. 6 Molybdenum Disulfide | Solvent #3/ MIL-L-23699 Oil 50/50 | Fl494 | Fl494 -42 & -43 | Photos Fl494-42 and -43 have metallic wear particles deposited on substrate. | Oil/solvent mixtures required to both solvate grease and suspend wear particles with some MoS ₂ type greases. |
| No. 8 Barium Complex Soap | Solvent #3 | Fl492 | Fl492 -44 to -46 | Wear particles identifiable in network of organic material. Heating Ferrogram 330°C (625°F) evaporates organic material. | Bichromatic illumination effective in identifying morphology of metal wear particles. |

TABLE 5. EXAMINATION OF SAMPLES TAKEN FROM GREASE-LUBRICATED SYSTEMS

| NO. | SOURCE | COMPONENT | NATURE OF SAMPLE | FERROGRAM NUMBER | REMARKS |
|-----|---------------------------|--|--|---------------------|--|
| 1 | E2 Grumman Aircraft | landing gear nosewheel tapered roller bearing | residual grease | F1940 | metallic particles probably initial contamination - residual soap appears as translucent material |
| 2 | E2 Grumman Aircraft | landing gear nosewheel tapered roller bearing | grease removed from race | F1943 | low wear metal concentration - oxides and compounds may be wear associated but bearing appears normal |
| 3 | F4 Landing Wheel | tapered roller bearing outer race | grease from race surface | F1964 | Ferrogram free of residual grease - few metallic particles ($>10 \mu\text{m}$) |
| 4 | H53 Helicopter | swash plate 353 hours since overhaul | outside of seal - probably residue of fill | F1965 | heavily contaminated with particles of carbonaceous appearance indica- tive of grease deterioration |
| 5 | H53 Helicopter | swash plate 353 hours since overhaul | from behind spacer | F1946 | many severe wear particles - 100 - 150 μm long |
| 6 | H53 Helicopter | swash plate 353 hours since overhaul | upper bearing around ball | F1966 | heavy deposit of friction polymer |
| 7 | H53 Helicopter | swash plate 353 hours since overhaul | upper bearing around ball, but opposite side | F1967 | debris is primarily friction polymer |
| 8 | H53 Helicopter | swash plate 353 hours since overhaul | from bearing edge | F1968 | rubbing wear some particles show blue |

(continued ...)

Table 5 (continued)

| NO. | SOURCE | COMPONENT | NATURE OF SAMPLE | FERROGRAM NUMBER | REMARKS |
|-----|-------------------|--|---|---------------------|---|
| 9 | H53 Helicopter | swash plate 353 hours since overhaul | from bearing edge but without edge grease | F1969 | very few normal rubbing particles are present - Ferrogram dominated by non-metallic crystalline debris which is rose colored in polarized light |
| 10 | H53 Helicopter | swash plate 353 hours since overhaul | lower bearing inside edge | F1970 | normal rubbing wear and friction polymers present - also, some non- metallic crystalline debris as seen on F1969, but in much lower quantity. |
| 11 | H53 Helicopter | swash plate 353 hours since overhaul | between two ball bearings (lower) | F1975 | brown non-metallic crystalline debris as in F1969 and F1970 after subsection to heat and pressure - normal rubbing wear particles, red oxide particles, and copious friction polymers present |
| 12 | H53 Helicopter | swash plate 353 hours since overhaul | between two ball bearings (lower) | F1977 | same as Ferrogram F1975, but deposit is lighter |
| 13 | Helicopter | reduction gear | from crack in gearbox housing | F1978 | light deposit, normal rubbing wear with just a few severe wear particles and little else |
| 14 | Helicopter | reduction gear | from minor gear teeth | F1979 | negligible wear, same as F1978, but fewer and smaller particles |
| 15 | Helicopter | reduction gear | same as 13 but not at crack | F1980 | negligible wear, same as F1978, but fewer and smaller particles |

(continued ...)

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Table 5 (continued)

| NO. | SOURCE | COMPONENT | NATURE OF SAMPLE | FERROGRAM NUMBER | REMARKS |
|-----|-------------------|--|---|---|--|
| 16 | Helicopter | reduction gear | from gear support bearing (Journal) | F1957 | severe and cutting wear particles, normal rubbing wear, and friction polymers - heavy deposit on Ferro- gram - not similar to F1978, F1979 or F1980 |
| 17 | Helicopter | reduction gear | planetary gear teeth | F1958 | cutting wear and severe wear par- ticles - large particles of friction polymer - normal rubbing wear particles - non-ferrous metal particles (cutting and severe wear) deposited along length of Ferrogram |
| 17 | Helicopter | reduction gear | planetary gear teeth 10:1 dilu- tion of above | F1986 | |
| 18 | H46 Helicopter | reduction gear | from gear support regions | F1959 | heavy deposits of friction polymer and severe wear particles many and large cutting wear particles |
| 18 | H46 Helicopter | reduction gear | from gear support regions | F1987 10:1 dilu- tion of above | |
| 19 | H46 Helicopter | stationary splines at rotor head | from below bottom spline | F1960 | low aspect ratio, rather thick, severe wear particles - non-ferro- magnetic - dark, metallo-oxide particles, red oxides, friction polymers, and normal rubbing wear |

(continued ...)

Table 5 (continued)

| NO. | SOURCE | COMPONENT | NATURE OF SAMPLE | FERROGRAM NUMBER | REMARKS |
|-----|--------------------|--|-------------------------|---------------------|--|
| 20 | H46 Helicopter | stationary splines at rotor head | off spline surfaces | F1961 | severe wear particles, dark metallo-oxides, red oxides, normal rubbing wear, fatigue chunks (many of which are non-ferromagnetic and non-metallic crystalline debris - rather heavy deposit) |
| 21 | H46 Helicopter | stationary splines at rotor head | off spline surfaces | F1962 | same as Ferrogram F1961, but deposit is not as heavy |
| 22 | CH 53A Aircraft | tail rotor spline | directly from spline | F1990 | very heavily particle laden friction polymers, dark metallo-oxides, with very little else |
| 23 | CH 53A Aircraft | tail rotor spline | directly from spline | F1991 | very heavily particle laden friction polymers, dark metallo-oxides, with very little else |

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Photo No. F1428-1 Magnification: 100X

Location on
Ferrogram: Entry (edge)

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium Soap

Solids: None

Solvent Type: Solvent #1

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Dissolved in 10 cc grease Solvent #1.
Typical example of undissolved grease/soap
mixture.



Photo No. F1428-2 Magnification: 100X

Location on
Ferrogram: Entry

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #1

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Another view of the undissolved
grease/soap mixture using Solvent #1.



Photo No. F1428-3 Magnification: 100X

Location on
Ferrogram: @ 41 mm

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #1

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Large mass of organic material thought to be lithium soap. Highly polar solvent systems are ineffective in dissolving this material.



Photo No. F1428-4 Magnification: 100X

Location on
Ferrogram: @ 41 mm

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #1

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Bichromatic light photo of same material in Photo F1428-3 above. Shows chiefly amorphous nature of undissolved grease.



Photo No. F1428-5 Magnification: 100X

Location on Ferrogram: Entry area

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #1

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Polarized light photo shows chiefly amorphous nature of undissolved grease. Some minor particulate matter present.



Photo No. F1428-6 Magnification: 100X

Location on Ferrogram: @ 35 mm

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #1

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Another view down the Ferrogram of material thought to be lithium soap apparently swollen by Solvent #1.

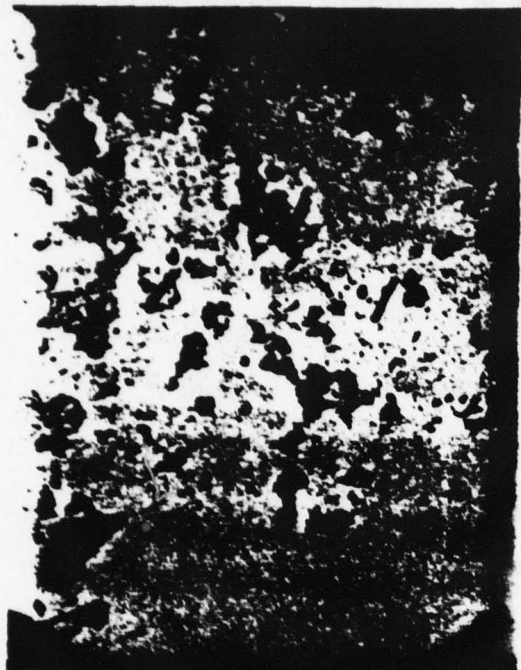


Photo No. F1437-7 Magnification: 100X

Location on
Ferrogram: Entry area

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Sample dissolved in grease Solvent #3,
(high aliphatic content). Good solvation.
No grease or soap evident. Some thin
non-metallic particulate matter present.

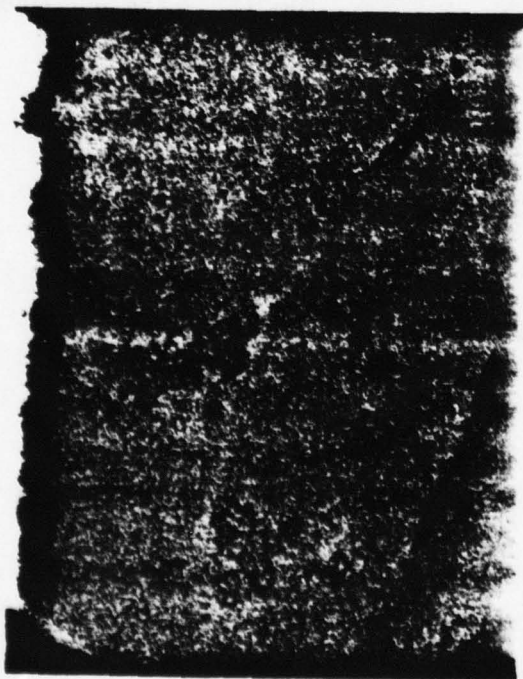


Photo No. F1437-8 Magnification: 100X

Location on
Ferrogram: Entry area

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Another view of same Ferrogram.
Emphasizes good solvent power of
Solvent #3 vs. Solvent #1 (Photos -1 to -6).

Photo No. F1478-9 Magnification: 100X

Location on
Ferrogram: Entry area

Grease Sample: #2

Lubricant Base: Petroleum

Thickener: Lithium

Solids: Molybdenum disulfide

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

All grease and soap solubilized.
Blue/black particles are MoS_2 ,
non-metallic spheres are
unknown material.

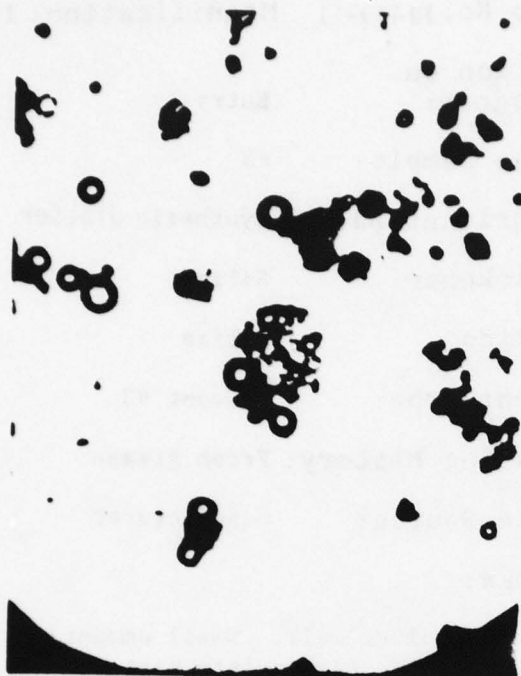


Photo No. F1478-10 Magnification: 100X

Location on
Ferrogram: Entry area

Grease Sample: #2

Lubricant Base: Petroleum

Thickener: Lithium

Solids: Molybdenum disulfide

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Bichromatic light photo of same
view as in Photo No. F1478-9 above
demonstrates transparent spheres
are non-metallic.

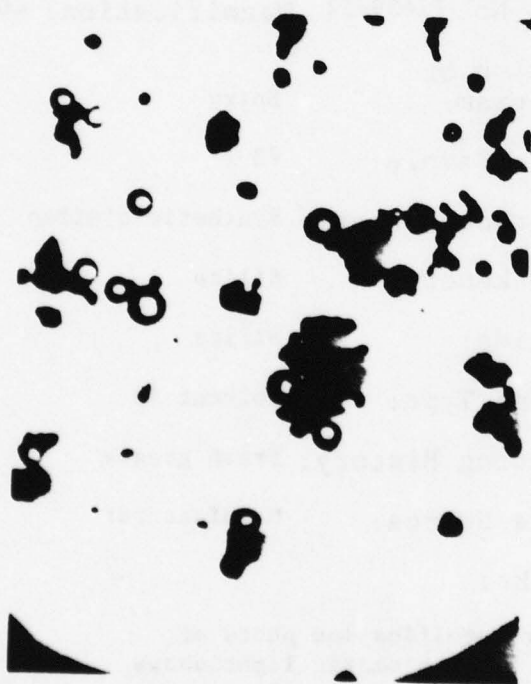




Photo No. F1439-11 Magnification: 100X

Location on
Ferrogram: Entry

Grease Sample: #3

Lubricant Base: Synthetic diester

Thickener: Silica

Solids: Silica

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Grease dissolved well. Small amount
of non-metallic particulate matter
present (silica).

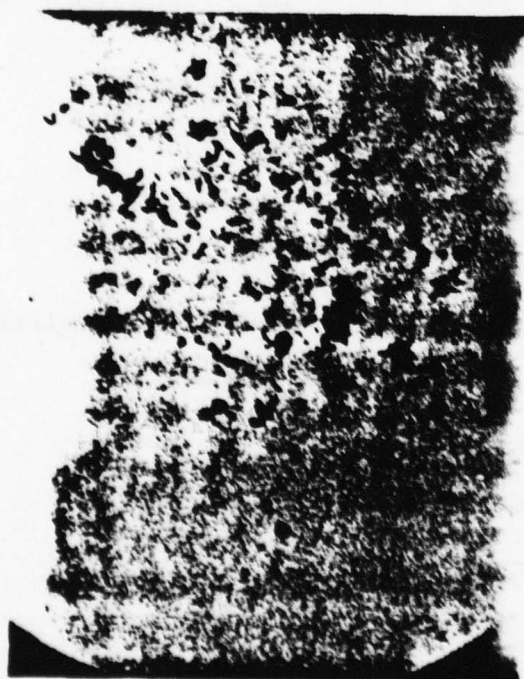


Photo No. F1439-12 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #3

Lubricant Base: Synthetic diester

Thickener: Silica

Solids: Silica

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Higher magnification photo of
F1439 in bichromatic light shows
the fine silica particles.

Photo No. F1442-13 Magnification: 100X



Location on
Ferrogram: Entry

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks: Some metal particles. Most of deposit is a high concentration of soap materials used in this type of grease. The used silicone greases show an entirely different deposit and these agglomerates disappear under heat and pressure.

Photo No. F1442-14 Magnification: 400X



Location on
Ferrogram: Entry

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

An enlarged view of Photo F1442-13 above.



Photo No. F1442-15 Magnification: 100X

Location on
Ferrogram: @ 51.5 mm

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Polarized light photo shows typical agglomerated particles found in this type of fresh silicone grease.



Photo No. F1442-16 Magnification: 400X

Location on
Ferrogram: @ 51.5 mm

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Magnified (400X) view of polarized light Photo F1442-15 circled above. No evidence of such structures in used silicone greases. See Photos F1491-36 and F1491-37.

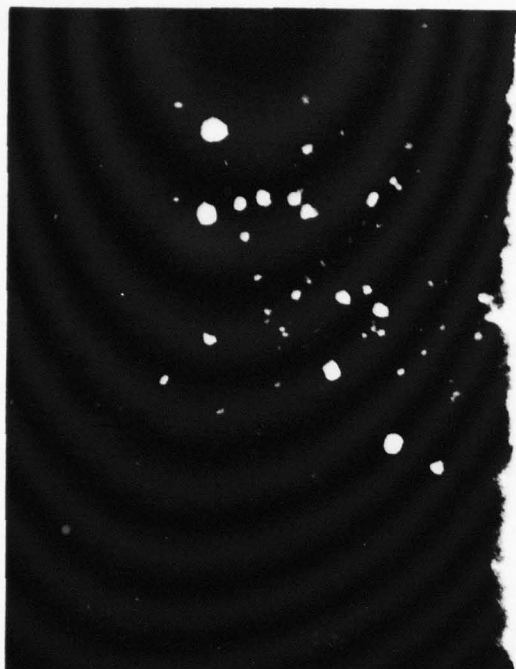


Photo No. F1442-17 Magnification: 100X

Location on
Ferrogram: Entry (edge)

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

This sample diluted 5:1 with Solvent #3.
Large soap particles much reduced in size
compared to original sample shown in
Photos F1442-13 to -16.

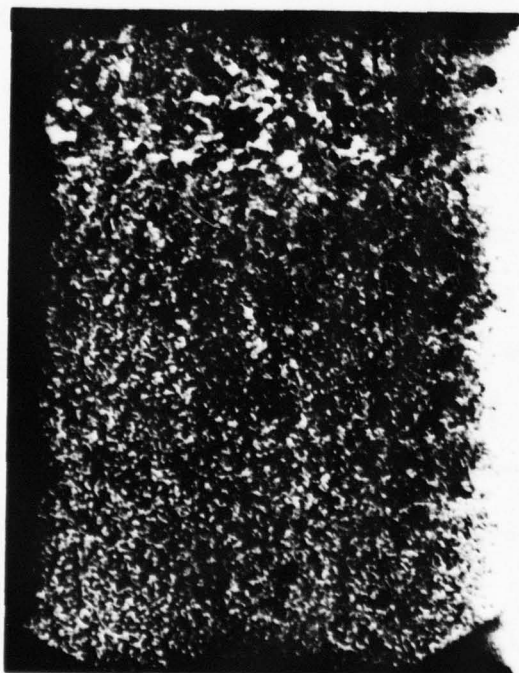


Photo No. F1442-18 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Enlarged view (400X) in bichromatic light
of diluted (5:1) fresh silicone grease
sample shows how particles are dispersed.

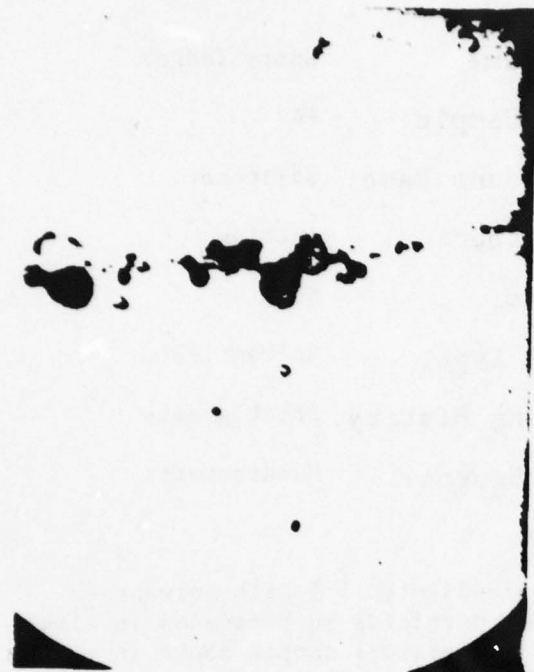


Photo No. F1434-19 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #5

Lubricant Base: Petroleum

Thickener: Aluminum complex

Solids: None

Solvent Type: Solvent #2

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Sample dissolved in 10 cc of grease Solvent #2. Metallic and non-metallic debris occluded with undissolved grease. Compare to F1438-20 below dissolved with grease Solvent #3.



Photo No. F1438-20 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #5

Lubricant Base: Petroleum

Thickener: Aluminum Complex

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Sample dissolved with grease Solvent #3. Except for minor amounts of metallic and non-metallic debris, substrate free of grease. Grease Solvent #3 clearly more effective than Solvents #1 and #2.

Photo No. F1440-21 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #6

Lubricant Base: Petroleum

Thickener: Mixed metal soap

Solids: Molybdenum disulfide

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Sample dissolved in 10 cc grease Solvent #3.
All MoS_2 particles settled in sample bottle
or turret tube. Only minor amounts
deposited on substrate.

Photo No. F1444-22 Magnification: 100X

Location on
Ferrogram: Entry

Grease Sample: #6

Lubricant Base: Petroleum

Thickener: Mixed Metal Soap

Solids: Molybdenum disulfide

Solvent Type: Solvent #3/MIL-L-23699,
50/50

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Sample dissolved in a 50/50 mixture of
Solvent #3 and MIL-L-23699 in order to
suspend MoS_2 particles. Compare to
Ferrogram F1440-21 above.



Photo No. F1444-23 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #6

Lubricant Base: Petroleum

Thickener: Mixed metal soap

Solids: Molybdenum disulfide

Solvent Type: Solvent #3/MIL-L-23699
50/50

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Enlarged view (400X) of Photo F1444-22.
Some particles exceed 50 μ m. MoS_2
particles have entirely different
configuration in used greases.

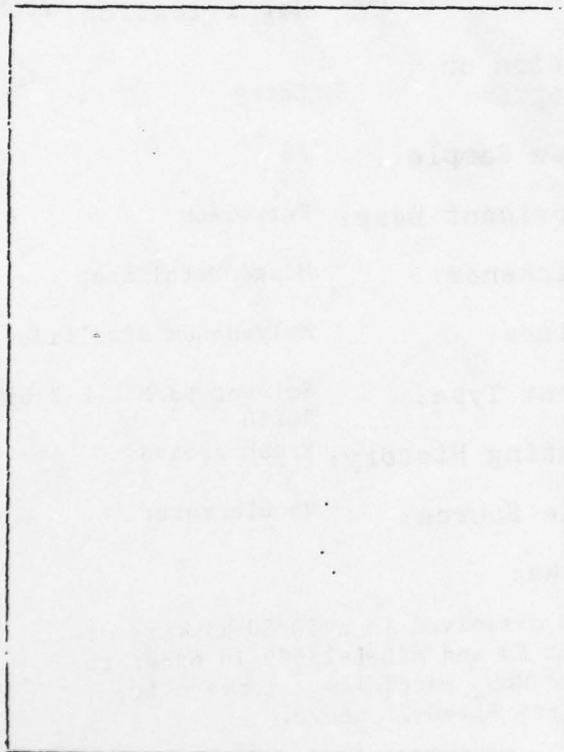


Photo No. Magnification:

Location on
Ferrogram:

Grease Sample:

Lubricant Base:

Thickener:

Solids:

Solvent Type:

Operating History:

Sample Source:

Remarks:



Photo No. F1441-24 Magnification: 400X

Location on
Ferrogram: Entry (edge)

Grease Sample: #7

Lubricant Base: Petroleum

Thickener: Clay (Bentone)

Solids: Molybdenum disulfide

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

MoS₂ particles smaller in size than in grease sample #6. Entry area shows a mixture of MoS₂ and clay.



Photo No. F1441-25 Magnification: 400X

Location on
Ferrogram: Entry (edge)

Grease Sample: #7

Lubricant Base: Petroleum

Thickener: Clay (Bentone)

Solids: Molybdenum disulfide

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Same as Photo F1441-24, but in bichromatic light. Differences between Bentone particles (transparent) and MoS₂ (red).

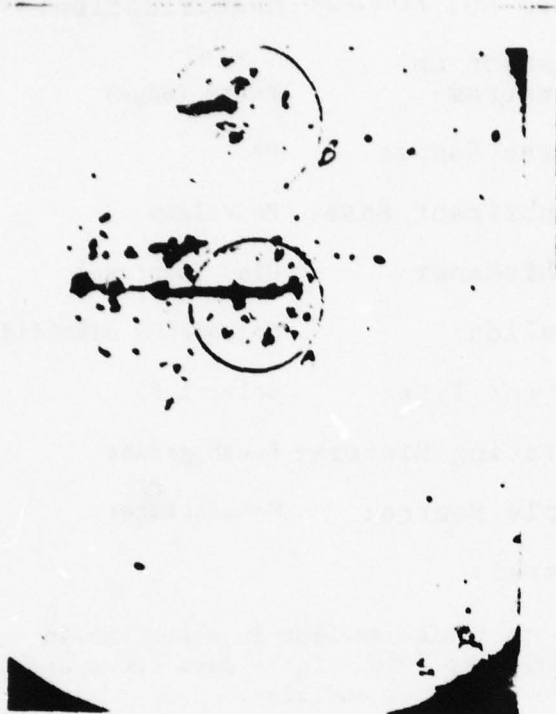


Photo No. F1443-26 Magnification: 100X

Location on Ferrogram: Entry

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Locations A & B (circles) show metallic particles caught in web-like mass. Composition unknown.



Photo No. F1443-27 Magnification: 400X

Location on Ferrogram: @ 51.5 mm

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

Solvent Type: Solvent #3

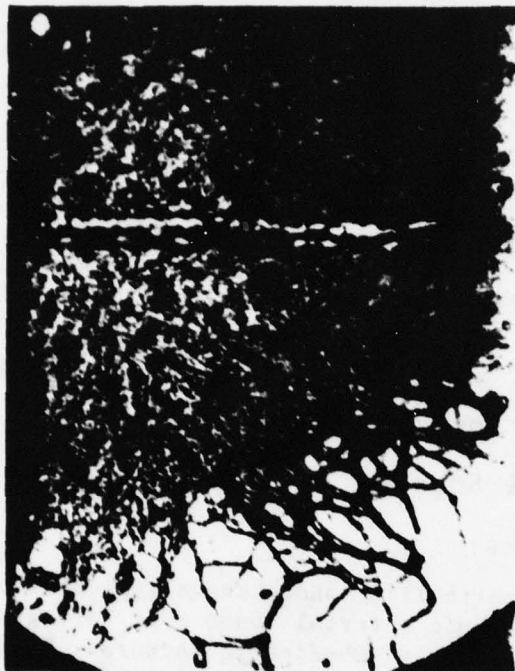
Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Web-like deposit away from entry area @ 51.5 mm.

Photo No. F1443-28 Magnification: 400X



Location on
Ferrogram: Re: Circle "A" on Photo
No. F1443-26

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Large (200 μ m) metal particle in large
network-like mass of organic material.

Photo No. F1443-29 Magnification: 400X



Location on
Ferrogram: Same as above

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Ferrogram F1443 heated to 625°F, 90 seconds.
Organic material fuses and shrinks.
Blue portion of metal (arrow) indicates
low carbon steel.



Photo No. F1443-30 Magnification: 400X

Location on Ferrogram: @ 54.6 mm

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Bichromatic light photo shows typical web-like organic material found over Ferrogram. Metal particle imbedded in network. This is typical of contamination in this grease sample.

Photo No. F1443-31 Magnification: 400X

Location on Ferrogram: @ 54.6 mm (same as photo F1443-30 above)

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Ferrogram heated to 625°F for 90 seconds. Blue (temper color) of metal indicates low alloy steel. Web-like material evaporated by heat. Most other greases and soaps withstand this heat treatment. See next Photo (No. F1423-32) lithium type grease heated in same manner.

Photo No. F1423-32 Magnification: 100X

Location on
Ferrogram: @ 54.4 mm

Grease Sample: #1

Lubricant Base: Petroleum

Thickener: Lithium

Solids: None

Solvent Type: Solvent #1

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

The undissolved lithium type grease on the Ferrogram heated to 625°F for 90 seconds. Some smoke evolved from the heat, but otherwise remains stable.



Photo No. F1479-33 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

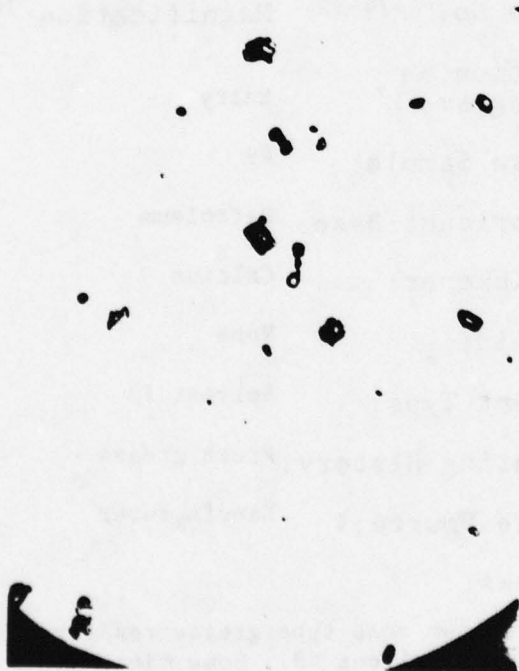
Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Barium complex type grease diluted 10:1. Much of the web-like organic material is dispersed.



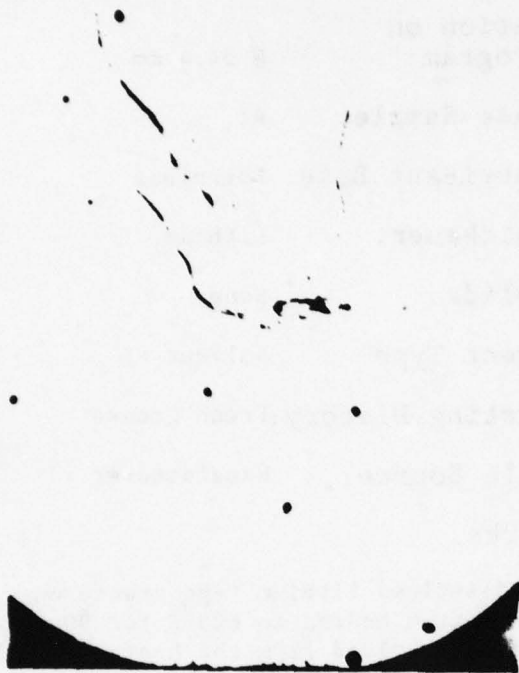


Photo No. F1479-34 Magnification: 400X

Location on Ferrogram: @ 54.7 mm

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium Complex

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

Same Ferrogram as F1479-33, but below entry (diluted 10:1). Small metal particle easily observable despite web or organic material.



Photo No. F1474-35 Magnification: 100X

Location on Ferrogram: Entry

Grease Sample: #9

Lubricant Base: Petroleum

Thickener: Calcium

Solids: None

Solvent Type: Solvent #3

Operating History: Fresh grease

Sample Source: Manufacturer

Remarks:

This calcium soap type grease readily soluble in Solvent #3. Some minor amount of debris (dirt) in entry area.



Photo No. F1491-36 Magnification: 100X

Location on Ferrogram: Entry

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Used grease, AISI 52-100 ball bearing & race, 80 PSI, 2 minutes

Sample Source: Manufacturer

Remarks:
Metallic wear particles easily visible in Bichromatic light. Mass of agglomerated particulate matter (see Photos No. F1442, -15 & -16) greatly reduced by wear tester action.



Photo No. F1491-37 Magnification: 400X

Location on Ferrogram: Entry

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Used grease, same as above.

Sample Source: Manufacturer

Remarks:
Enlarged view (400X) of entry deposit in Bichromatic light. Demonstrates that large amount of soap material in used silicone grease present low interference when observing metal particles microscopically.



Photo No. F1491-38 Magnification: 400X

Location on Ferrogram: Entry area

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Used grease same as F1491-38.

Sample Source: Manufacturer

Remarks:

Another view in Bichromatic light showing contrast between metallic wear particles and non-metallic debris.

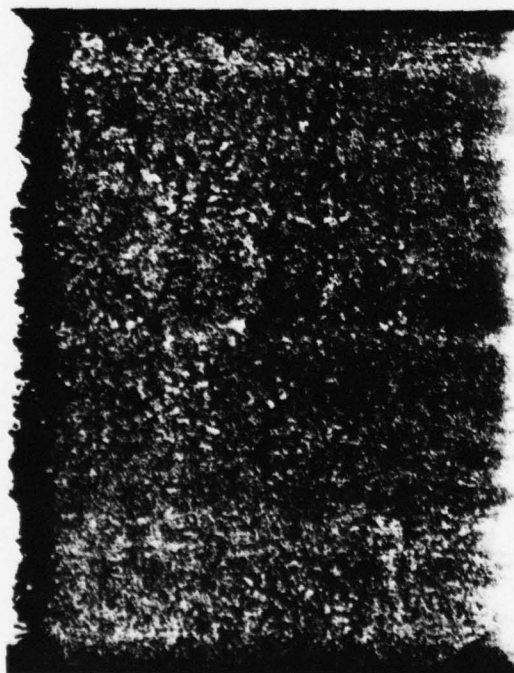


Photo No. F1491-39 Magnification: 400X

Location on Ferrogram: 54.5 mm

Grease Sample: #4

Lubricant Base: Silicone

Thickener: Lithium

Solids: None

Solvent Type: Solvent #3

Operating History: Used grease same as F1497-38.

Sample Source: Manufacturer

Remarks:

View of typical metallic wear particles down from entry area. These particles readily identifiable from non-metallic debris in background using Bichromatic light.

Photo No. F1493-40 Magnification: 100X

Location on
Ferrogram: Entry

Grease Sample: #6

Lubricant Base: Petroleum

Thickener: Mixed

Solids: Molybdenum disulfide
(large particle size)

Solvent Type: Solvent #3

Operating History: Used grease, AISI 52-
100 ball & race, 80 PSI, 2 minutes.

Sample Source: Manufacturer

Remarks:

Lack of any significant deposit of metal
caused by rapid settling in sample bottle.
Typical of MoS_2 greases.



Photo No. F1493-41 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #6

Lubricant Base: Petroleum

Thickener: Mixed

Solids: Molybdenum disulfide

Solvent Type: Solvent #3

Operating History: Used grease, same as
above.

Sample Source: Manufacturer

Remarks:

Isolated worn MoS_2 particle. Compare this
and Photo above to Photos F1494-42
where MIL-L-23699 oil was used to suspend
particles in solvent solution.

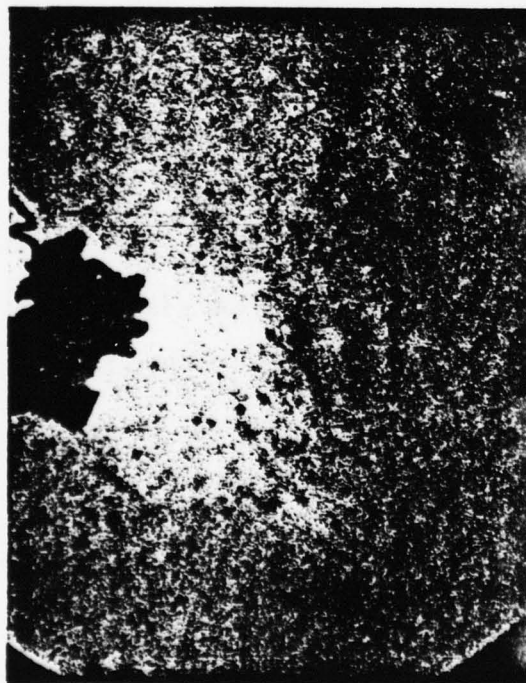




Photo No. F1494-42 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #6

Lubricant Base: Petroleum

Thickener: Mixed

Solids: Molybdenum disulfide
(large particles)

Solvent Type: Solvent #3

Operating History: Used grease, AISI 52-
100 ball bearing & race, 80 PSI, 2 minutes.

Sample Source: Manufacturer

Remarks:

Same grease sample as in Ferrogram F1493, but
Solvent #3 mixed 50/50 with MIL-L-23699 to
suspend wear particles. Metallic wear
particles readily observed on substrate.



Photo No. F1494-43 Magnification: 400X

Location on
Ferrogram: Entry

Grease Sample: #6

Lubricant Base: Petroleum

Thickener: Mixed

Solids: Molybdenum disulfide

Solvent Type: Solvent #3/ MIL-L-23699
50/50

Operating History: Used grease, as above.

Sample Source: Manufacturer

Remarks:

View of metallic wear particles
in Bichromatic light.



Photo No. F1492-44 Magnification: 100X

Location on Ferrogram: Entry

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium complex

Solids: None

Solvent Type: Solvent #3

Operating History: Used grease, AISI 52-100 ball bearing against race, 80 PSI, 2 min.

Sample Source: Manufacturer

Remarks:

General view of entry deposit in Bichromatic light. Very little interference from web-like deposit found in fresh barium greases in viewing metallic wear particles.

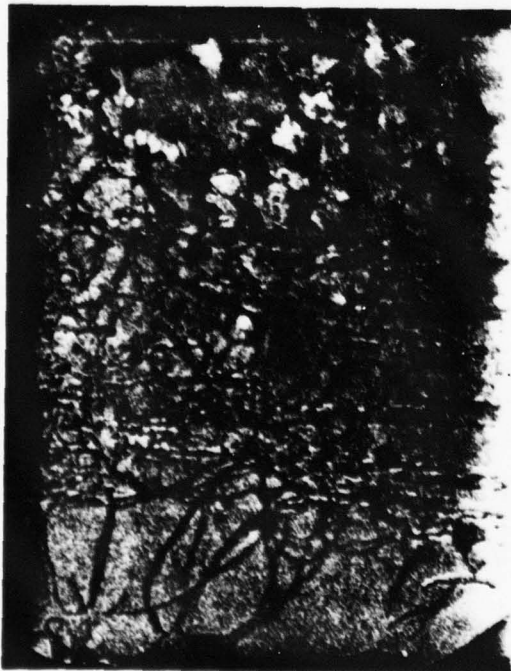


Photo No. F1492-45 Magnification: 400X

Location on Ferrogram: Entry (edge)

Grease Sample: #8

Lubricant Base: Petroleum

Thickener: Barium complex

Solids: None

Solvent Type: Solvent #3

Operating History: Used grease, as above.

Sample Source: Manufacturer

Remarks:

Enlarged (400X) Bichromatic light view of metallic wear particles against background of web-like organic material. See also heated Ferrogram (Photo No. F1492-46).



Photo No. F1492-46 Magnification: 400X

Location on

Ferrogram:

Entry

Grease Sample:

#8

Lubricant Base: Petroleum

Thickener:

Barium complex

Solids:

None

Solvent Type:

Solvent #3

Operating History: Used grease

Sample Source:

manufacturer

Remarks:

Ferrogram F1492 heated to 625°F for 90 seconds. Just as with fresh greases, organic network disappeared on heating, leaving metallic particles with typical blue oxide temper colors.

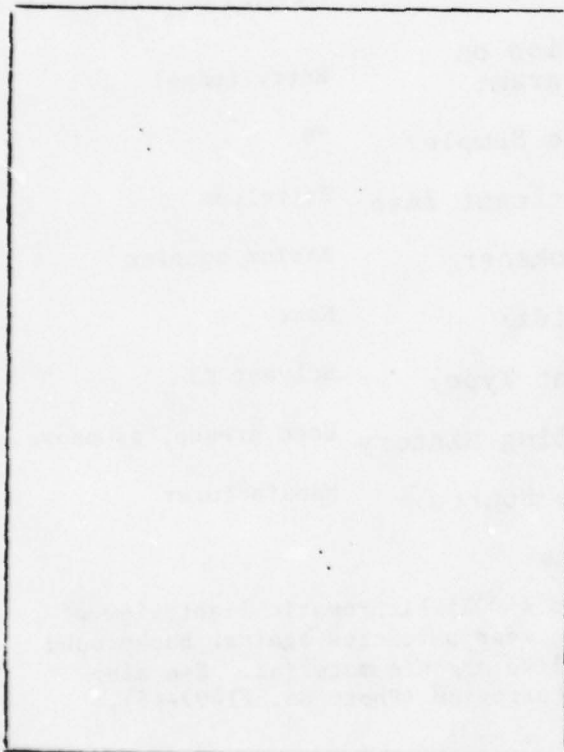


Photo No.

Magnification:

Location on

Ferrogram:

Grease Sample:

Lubricant Base:

Thickener:

Solids:

Solvent Type:

Operating History:

Sample Source:

Remarks:

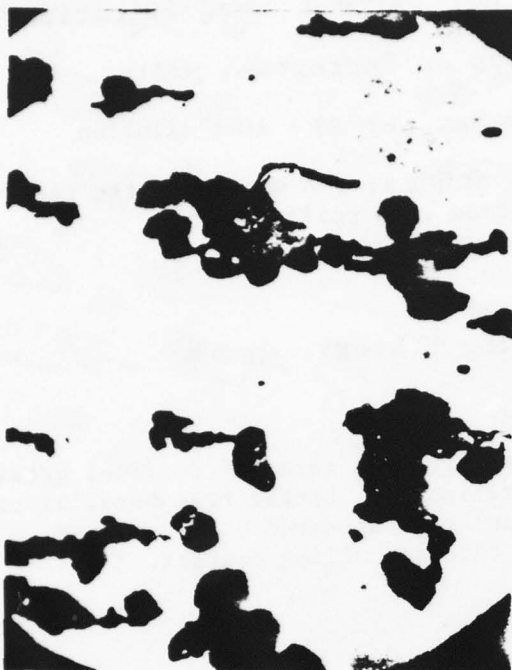


Photo No: F1940-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #1 - no dilution

Sample Source: Landing gear nosewheel of
E-2 Grumman two tapered roller bearings
residual grease.

Operating History: X

Remarks:

All debris, including metallic particles,
probably contamination of original grease
translucent material is residual soap.



Photo No: F1943-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #2 - no dilution

Sample Source:
Same bearing as above. Grease removed
from race.

Operating History: x

Remarks:

Low wear metal concentration. The primary
difference to the above reference sample
is the presence of oxides and compounds
that may be wear associated or contaminants.
Bearing appears normal



Photo No: F1964-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #3 10:1 dilution

Sample Source: F-4 wheel - outer race -
sample from race surface.

Operating History: x

Remarks:

Clean Ferrogram in terms of residual grease
and contaminants. Larger free metal particles
($> 10 \mu\text{m}$) give appearance of repeated
passage through rolling contact.

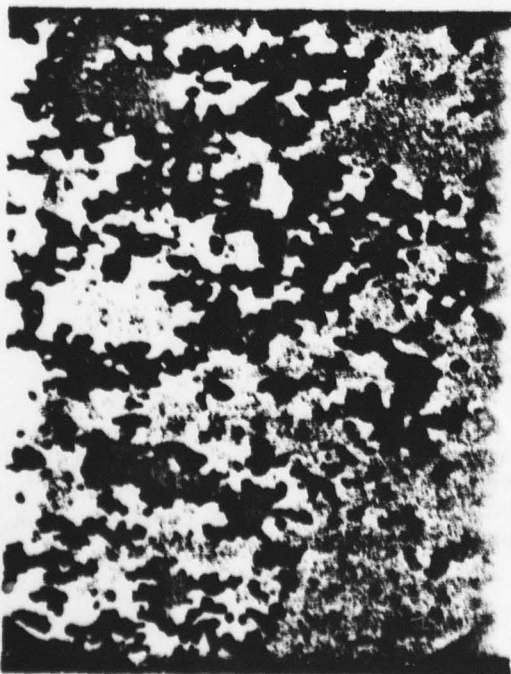


Photo No: F1965-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #4 100:1 dilution

Sample Source: Swash plate H53 helicopter.
Grease from outside of seal, possibly residue
of fitting grease.

Operating History:

Hours on unit: 1203 - Since overhaul: 353

Remarks:

Heavily contaminated.



Photo No: F1946-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #5 no dilution

Sample Source: Swash plate, H53 Helicopter.
Grease from behind spacer, probably has not
come in contact with rolling elements.

Operating History: hours on unit - 1203.
since overhaul - 353

Remarks:

Considering the sample source, there are
present a surprisingly large number of
severe wear particles.



Photo No: F1966-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #6 100:1 dilution

Sample Source: Swash plate, H53 Helicopter.
Grease from upper bearing around ball.
Probably some from bearing edge.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:

Heavy deposits of friction polymer.



Photo No: F1967-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #7 10:1 dilution

Sample Source: Swash plate, H53 helicopter.
From upper bearing around ball.
Opposite side from Sample #6.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:



Photo No: F1968-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #8 10:1 dilution

Sample Source: Swash plate H53 helicopter.
From the bearing edge (inside edge).

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:

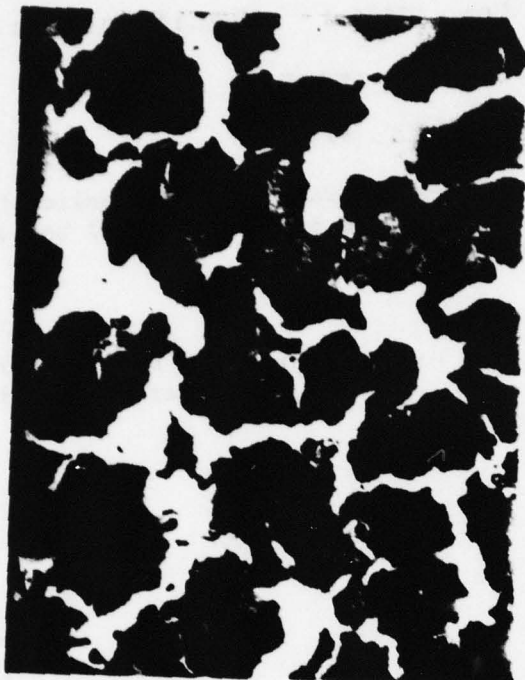


Photo No: F1969-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #9 10:1 dilution

Sample Source: Swash plate H53 helicopter.
Same as #7. Upper bearing around ball.
Attempted to clear edge grease sway.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:



Photo No: F1970-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #10 10:1 dilution

Sample Source: Swash plate H53 helicopter.
Lower bearing inside edge.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:

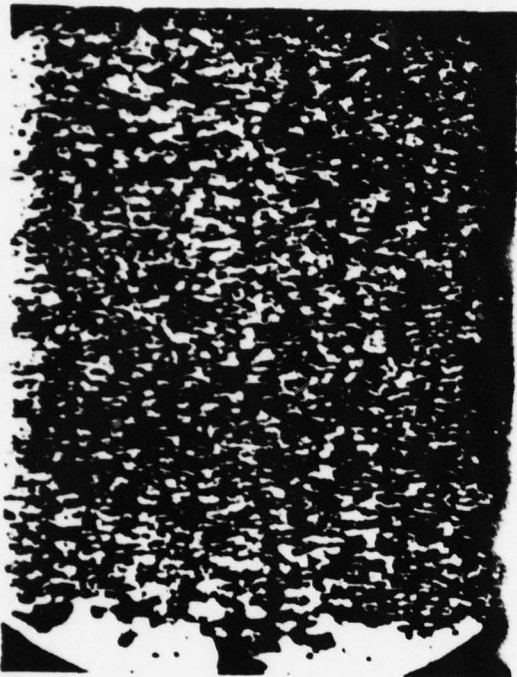


Photo No: F1975-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #11

Sample Source: Swash plate H53 helicopter.
Sample removed from between two ball bearings
(lower).

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:



Photo No: F1977-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #12 100:1 dilution

Sample Source:
Taken from same area as Sample #11 above.

Operating History: same as above

Remarks:



Photo No: F1978-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #13 100:1 dilution

Sample Source: Helicopter.
Reduction gear for rotor folding.
Sampled at crack in gear box housing.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:



Photo No: F1979-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #14 100:1 dilution

Sample Source: Helicopter
Reduction gear.
Sampled at gear teeth (minor gear)

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:

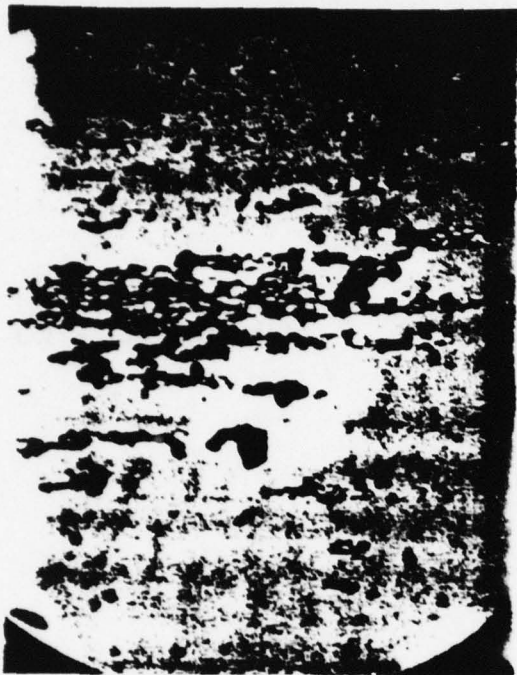


Photo No: F1980-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #15 100:1 dilution

Sample Source: Helicopter.

Reduction Gear. Sampled at gear teeth.

Similar to sample #13, but not at crack.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:



Photo No: F1957-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #16 not diluted

Sample Source: Helicopter.

Reduction Gear. Sample taken from
sliding bearing.

Operating History:

Remarks:

Heavy free metal deposits.



Photo No: F1958-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #17 not diluted

Sample Source: Helicopter
Reduction Gear. Sampled from planetary
gear teeth.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:



Photo No: F1986-1 Magnification: 1000x

Location on Ferrogram: edge of entry

Grease Sample: #17 10:1 dilution

Sample Source:

same as above

Operating History: same as above

Remarks:



Photo No: F1987-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #18 10:1 dilution

Sample Source: Helicopter
Reduction Gear. Sampled from gear support
region.

Operating History: hours on unit - 1203
since overhaul - 353

Remarks:



Photo No: F1959-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #18 no dilution

Sample Source: same as above

Operating History: same as above

Remarks:

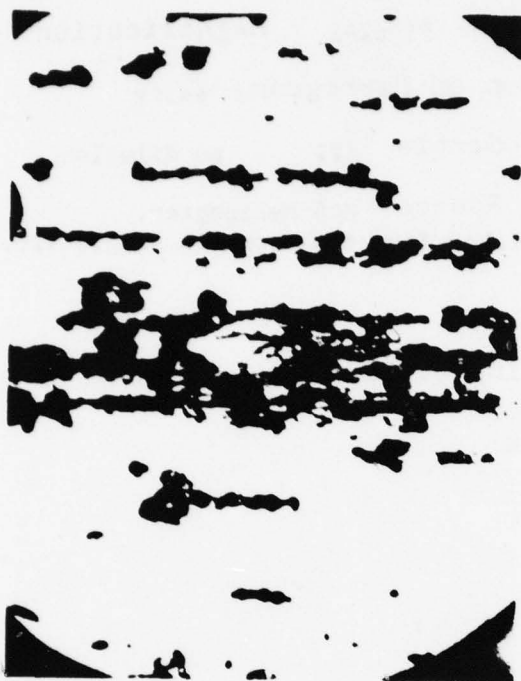


Photo No: F1960-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #19 no dilution

Sample Source: H46 Helicopter.
Stationary splines at rotor head.
Sample taken below bottom spline.

Operating History: not applicable

Remarks:



Photo No: F1961-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #20 no dilution

Sample Source: H46 Helicopter.
Stationary splines at rotor head.
Sample taken off spline surfaces.

Operating History: not applicable

Remarks:

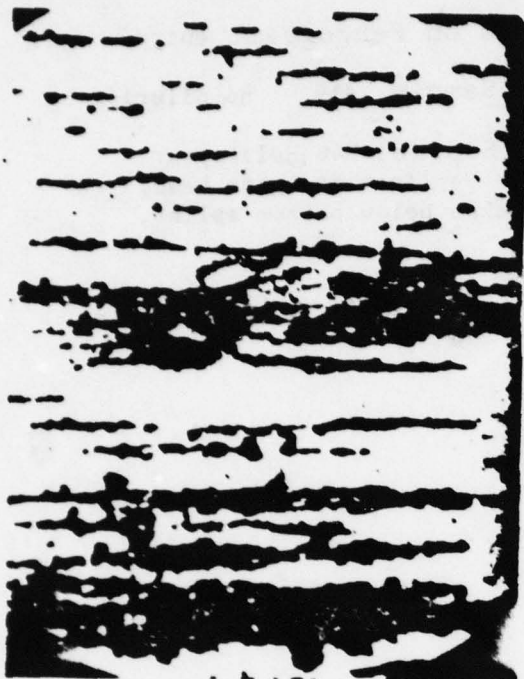


Photo No: F1962-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #21 no dilution

Sample Source: H46 helicopter.

Sample taken from same area as sample #20.

Operating History: not applicable

Remarks:

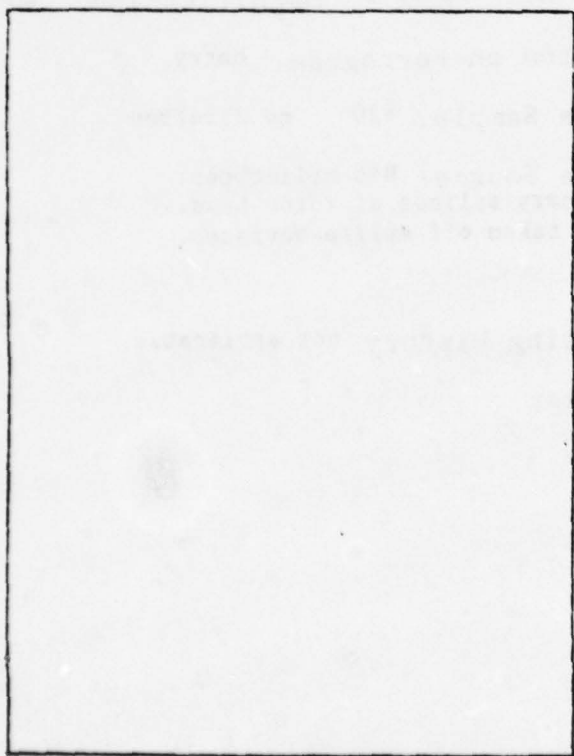


Photo No: Magnification:

Location on Ferrogram:

Grease Sample:

Sample Source:

Operating History:

Remarks:

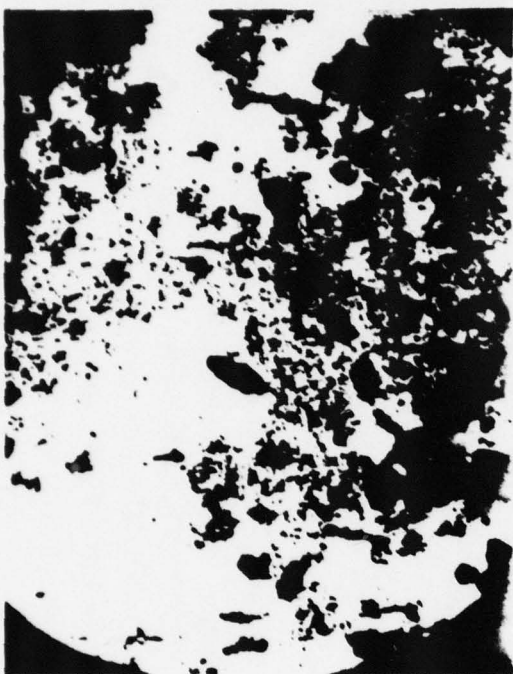


Photo No: F1990-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #22 100:1 dilution

Sample Source: CH 53A aircraft.
Tail rotor spline, sampled directly from
spline, open to environment in parked position.

Operating History: not applicable

Remarks:



Photo No: F1991-1 Magnification: 400x

Location on Ferrogram: entry

Grease Sample: #23 100:1 dilution

Sample Source: CH 53A aircraft.
Sample taken from same location as sample #22.
Appeared very dirty.

Operating History: not applicable

Remarks:

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P. Camberg
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Code 102
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San Diego, CA 92135

Mr. A. Cameron
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USAMC
DRCPM-IAP-T
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Naval Aviation Integrated Logistic
Support Center
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Attn: C. Chandler

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Leicester CE1 9BH UK

Mr. Collegeman
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(AIR-53645A)
Navy Dept.
Washington, DC 20361

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Bendix
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Dr. N. H. Cook
Massachusetts Institute of Technology
77 Massachusetts Avenue
Cambridge, MA 02139

A. S. Coolidge, Design Engineer
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